

# TRANSPORTPROZESSE &

## ERSTARRUNG

### ❖ **Transportprozesse**

- Diffusion
- Soret-Effekt
- Wärmeleitung

### ❖ **Erstarrung**

- Diffusives Wachstum
- Konstitutionelle Unterkühlung
- Thermosolutale Konvektion

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## DIFFUSION-THEORIE

Thermisch:  $j_T = -k \nabla T$  (Fourier)

Solutal:  $j_c = -D \nabla c$  (Fick)

Kontinuitätsgleichung:

$$\frac{\partial c}{\partial t} + \nabla j = 0$$

Diffusionsgleichung:

$$\frac{\partial c}{\partial t} = \nabla^2 c$$

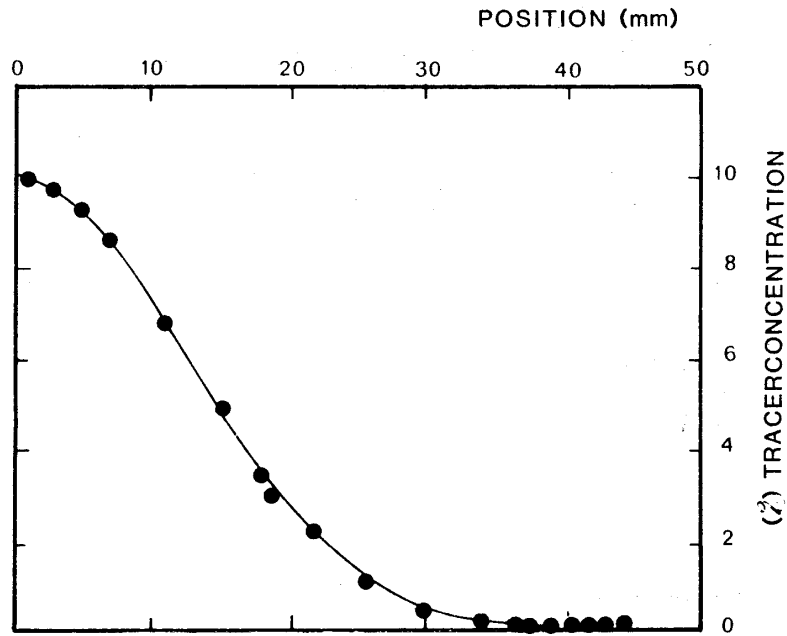
1-dimensionale Lösung:

$$c(x, t) = \frac{c_0 d}{\sqrt{\pi D t}} \exp\left(-\frac{x^2}{4 D t}\right)$$

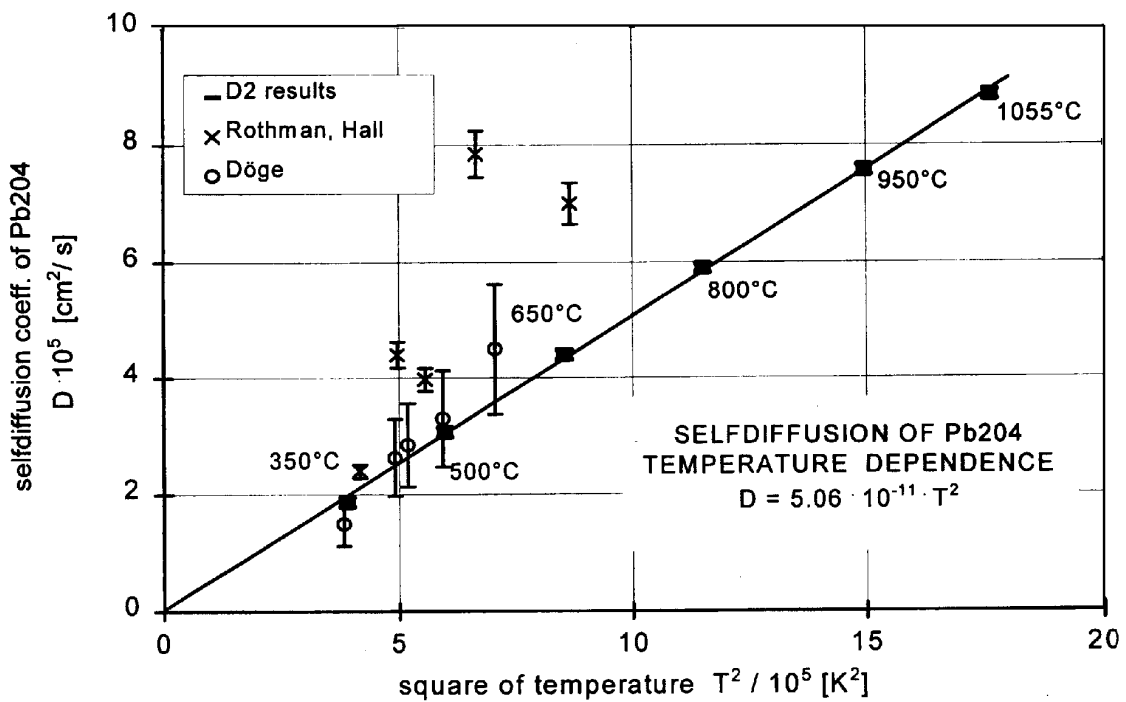
(Wärmetransport analog)



# DIFFUSION-EXPERIMENT



Concentration profile of Sn 112 (810°C, capillary y 1 mm Ø):  
Space Experiment (Frohberg, Kraatz, Wever)

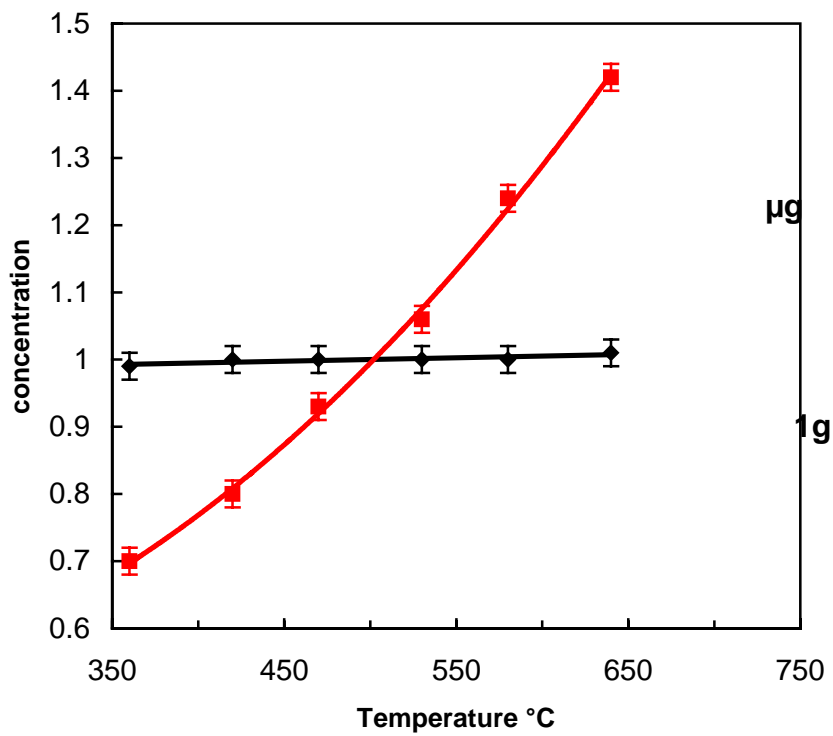


# SORET-EFFEKT

$$\frac{\partial c}{\partial t} = \nabla(D\nabla c + S\nabla T)$$



Soret effect Co in Sn,  $T_0 = 500 \text{ }^\circ\text{C}$



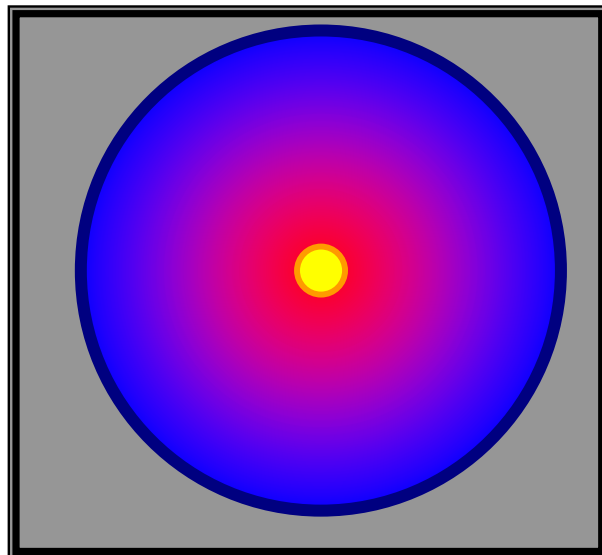
$$\nabla c = -\frac{S}{D} \nabla T$$



## WÄRMELEITUNG

$$\rho c_p \frac{\partial T}{\partial t} = k \nabla^2 T + \rho \dot{Q}_{ext}$$

Transient Hot Wire in Zylindergeometrie:



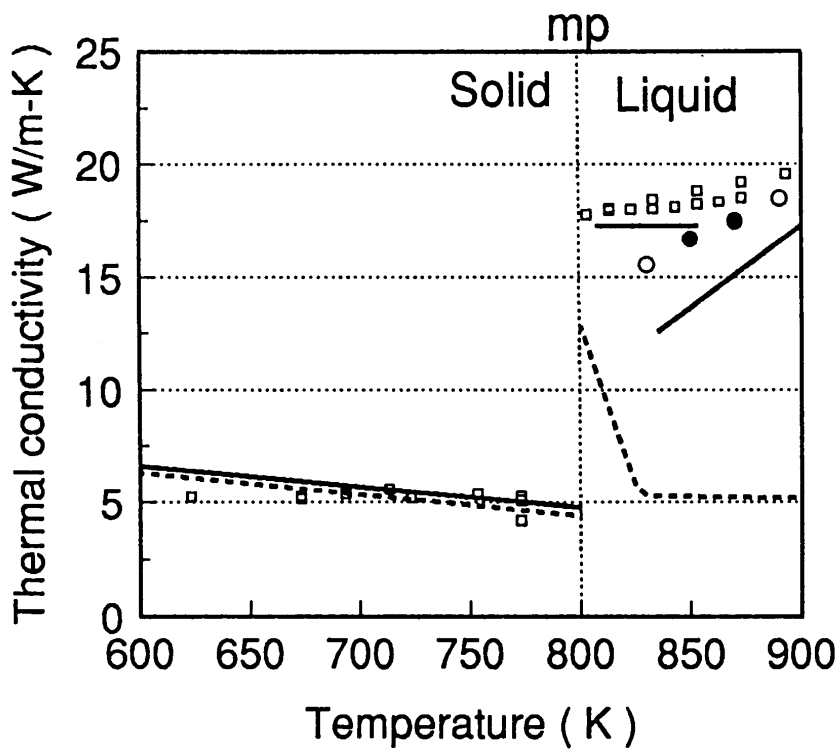
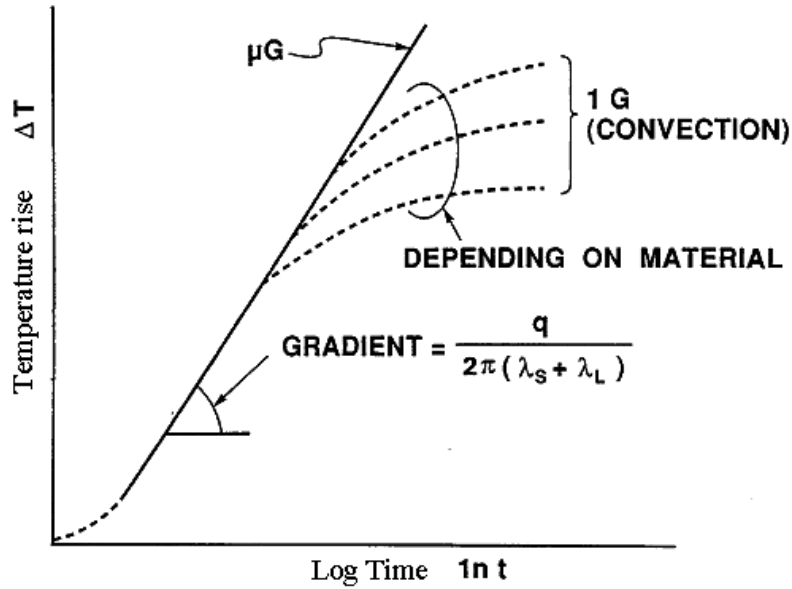
Randbedingung:  $\dot{Q}_{ext}(r, t) = \dot{q} \delta(r) \theta(t)$

Asymptotische Lösung:

$$\Delta T(R_0, t) = -\frac{\dot{q}}{4\pi k} \text{Ei}\left(-\frac{R_0^2}{4kt}\right) \approx \frac{\dot{q}}{4\pi k} \ln t$$



# WÄRMELEITUNG



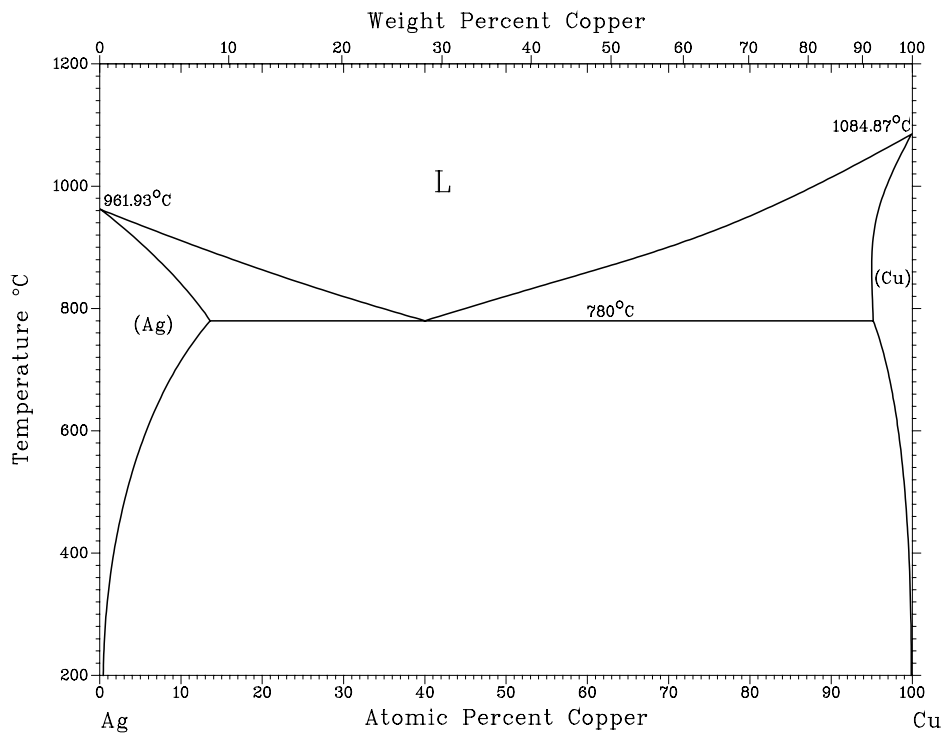
Drop shaft TEXUS-24 Terrestrial Amirkhanov Fedorov

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# ERSTARRUNG (1)

Typisches Phasendiagramm (Ag-Cu):



Verteilungskoeffizient:  $k = \frac{c_S}{c_L} < 1$

Konzentrationsüberschuss:

$$\Delta c = c_L - c_S = (1 - k)c_L$$



## ERSTARRUNG (2)

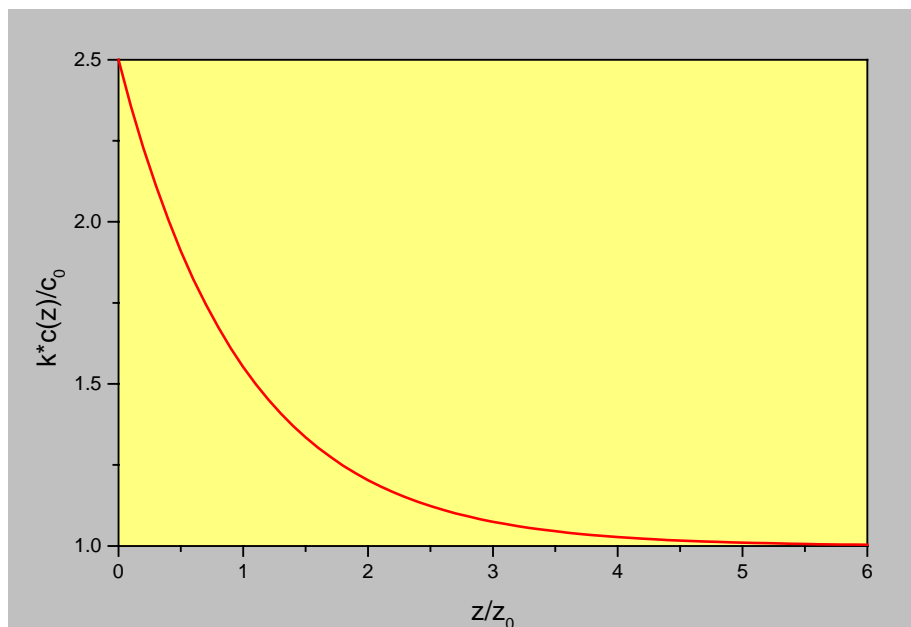
Stationäres Wachstum:  $\frac{\partial c}{\partial t} = 0$

$$v_0 \nabla c = D \nabla^2 c$$

1-dimensionale Lösung:

$$c(z) = c_0 \left( 1 + \frac{1-k}{k} \exp \left[ -\frac{v_0}{D} z \right] \right)$$

$$c(0_+) = c_0/k, \quad c(0_-) = kc(0_+) = c_0$$



## KONSTITUTIONELLE UNTERKÜHLUNG

Gerichtete Erstarrung:  $T(z) = T_0 + Gz$

Liquidustemperatur:  $T_L = T_L(c) \approx T_m - mc$

$c=c(z) \rightarrow T_L = T_L(z)$

Konstitutionelle Unterkühlung:

$$T(z_0) < T_L(z_0) \Leftrightarrow G < T_L'(0)$$

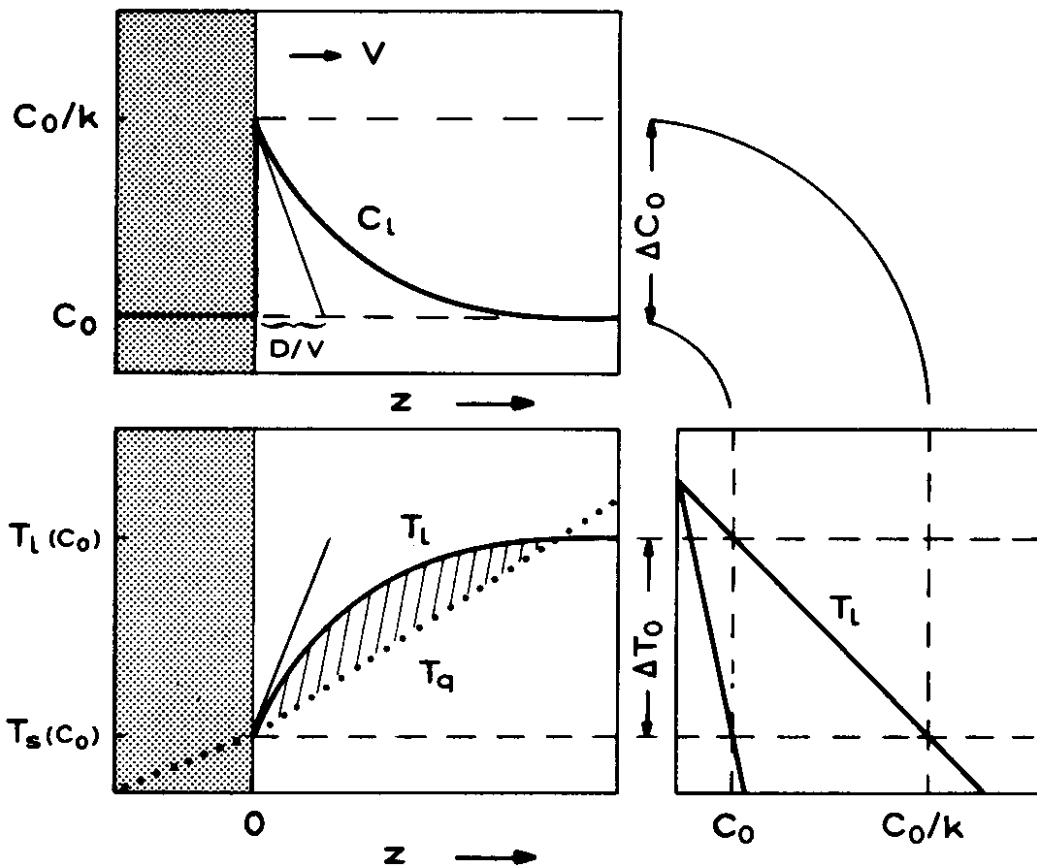
$$T_L'(0) = \left. \frac{dT_L}{dz} \right|_{z=0} = \frac{mc_0(1-k)v_0}{kD}$$

Rayleigh-Konvektion:

$$G > \frac{\kappa\eta Ra^c}{\rho\beta L^4 g} \Rightarrow \text{Mikrogravitation !}$$



# KONSTITUTIONELLE UNTERKÜHLUNG



# THERMOSOLUTALE KONVEKTION

1-dimensionale Betrachtung:

$$\frac{d\rho(c,T)}{dz} = \frac{\partial\rho}{\partial c} \frac{\partial c}{\partial z} + \frac{\partial\rho}{\partial T} \frac{\partial T}{\partial z}$$

$$\frac{\partial c}{\partial z} = -\frac{(1-k)v_0}{kD} \exp\left(-\frac{v_0 z}{D}\right) < 0, \quad \frac{\partial T}{\partial z} = G > 0$$

$$\frac{\partial\rho}{\partial c} = \alpha\rho, \quad \frac{\partial\rho}{\partial T} = -\beta\rho, \quad \beta > 0$$

⇒ Vorzeichenwechsel in  $d\rho/dz$ , falls

$$-\alpha \frac{(1-k)v_0}{kD} > \beta G, \text{ d.h. } \alpha < 0$$

⇒ keine stabile Schichtung möglich

⇒ Rayleigh-Konvektion für  $Ra > Ra^c$

⇒ **Mikrogravitation !**

