



# The Running Behaviour of an Elastic Wheelset

Ingo Kaiser

German Aerospace Center (DLR) Oberpfaffenhofen,  
Institute of Robotics and Mechatronics

**Karl Popp**

University of Hannover, Institute of Mechanics

---

# Outline

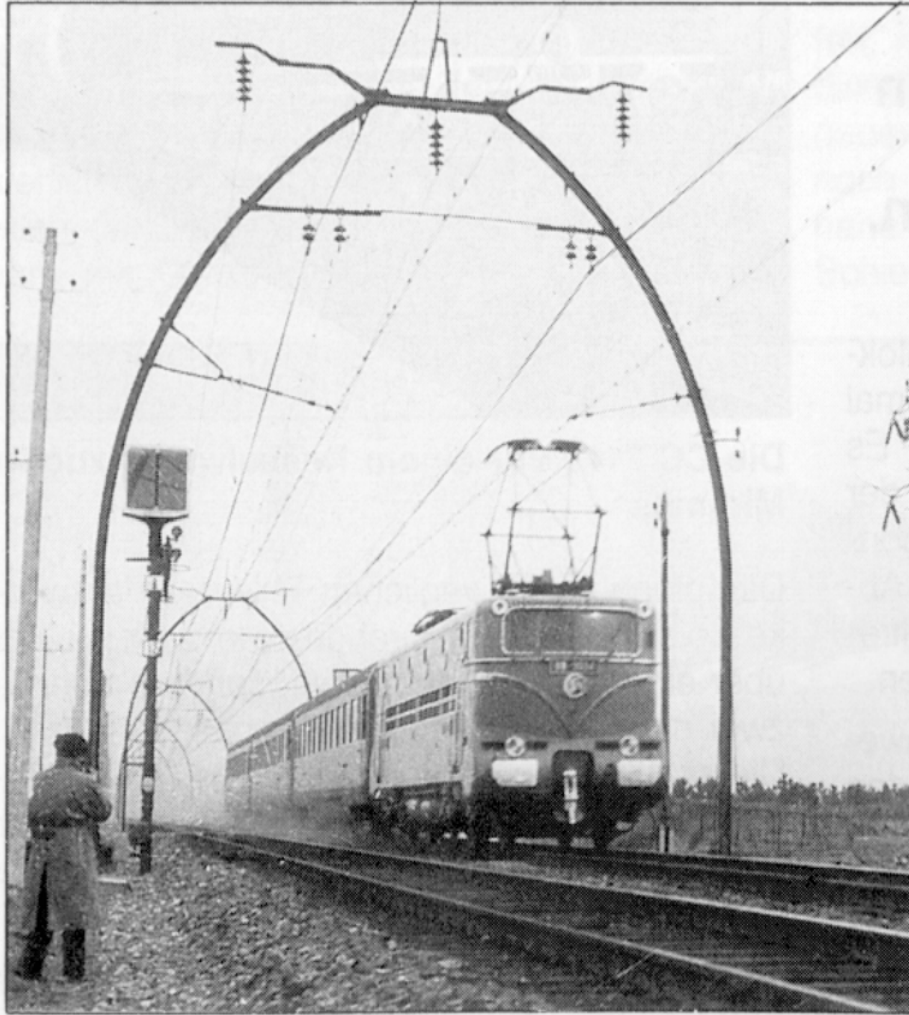
---

- **Introduction**
- **Modelling of the vehicle**
  - **Integration of the rotating elastic wheelsets**
  - **Structural dynamics of the wheelsets**
- **Modelling of the track**
  - **Structure of a track with discrete sleepers**
  - **Structural dynamics of the rails**
- **Simulation results: The influence of the structural elasticities**
- **Concluding remarks**



# Vehicle-track interaction

World speed record, 1955, 331 km/h, near Bordeaux



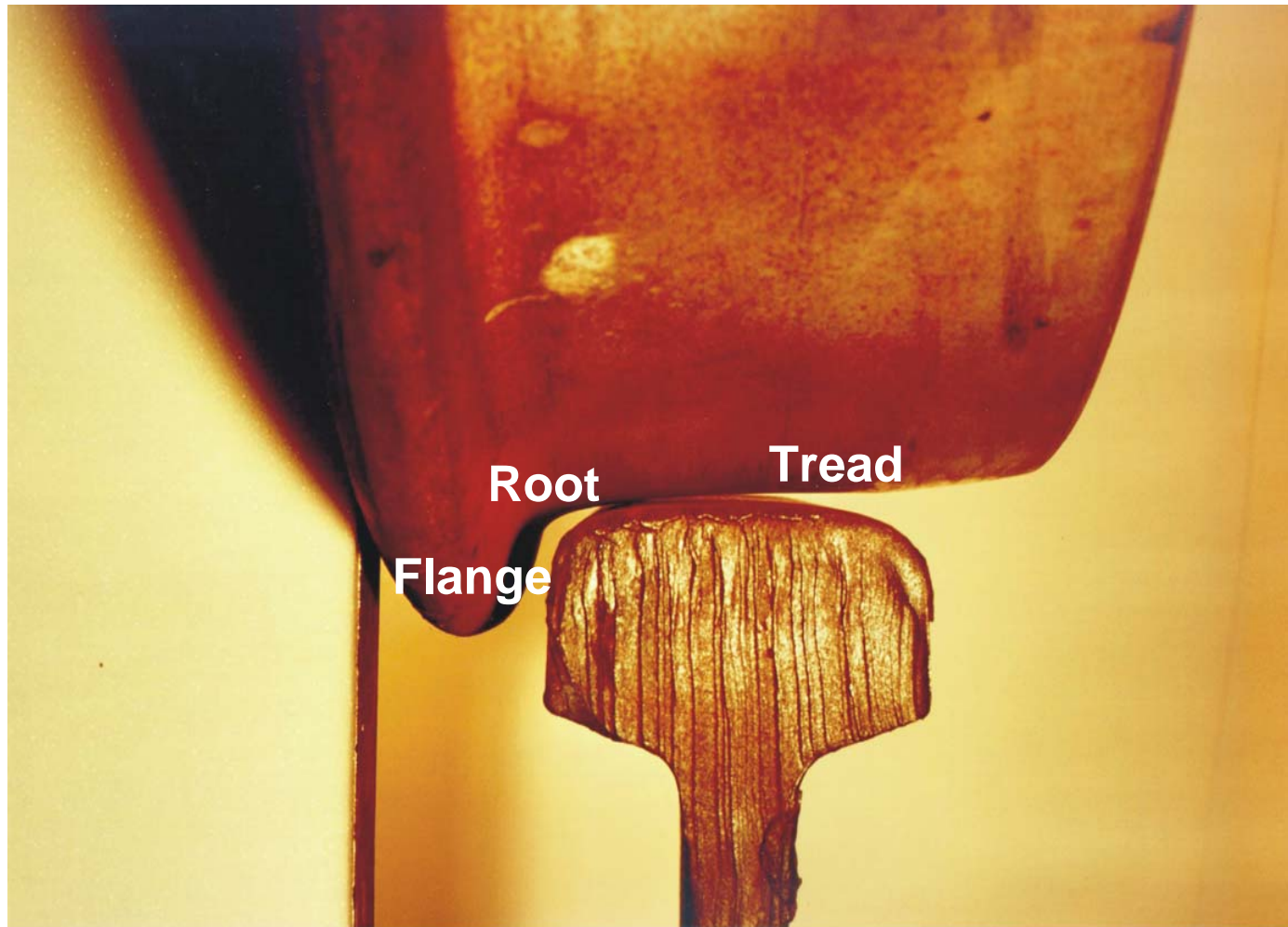
Source: eisenbahn-magazin 3/95 / SNCF / Sammlung Messerschmidt



Source: eisenbahn-magazin 3/95 / La Vie du Rail / Sammlung Hughes



# Real wheel-rail contact



Source: Institute for Railway Vehicles, University of Hannover



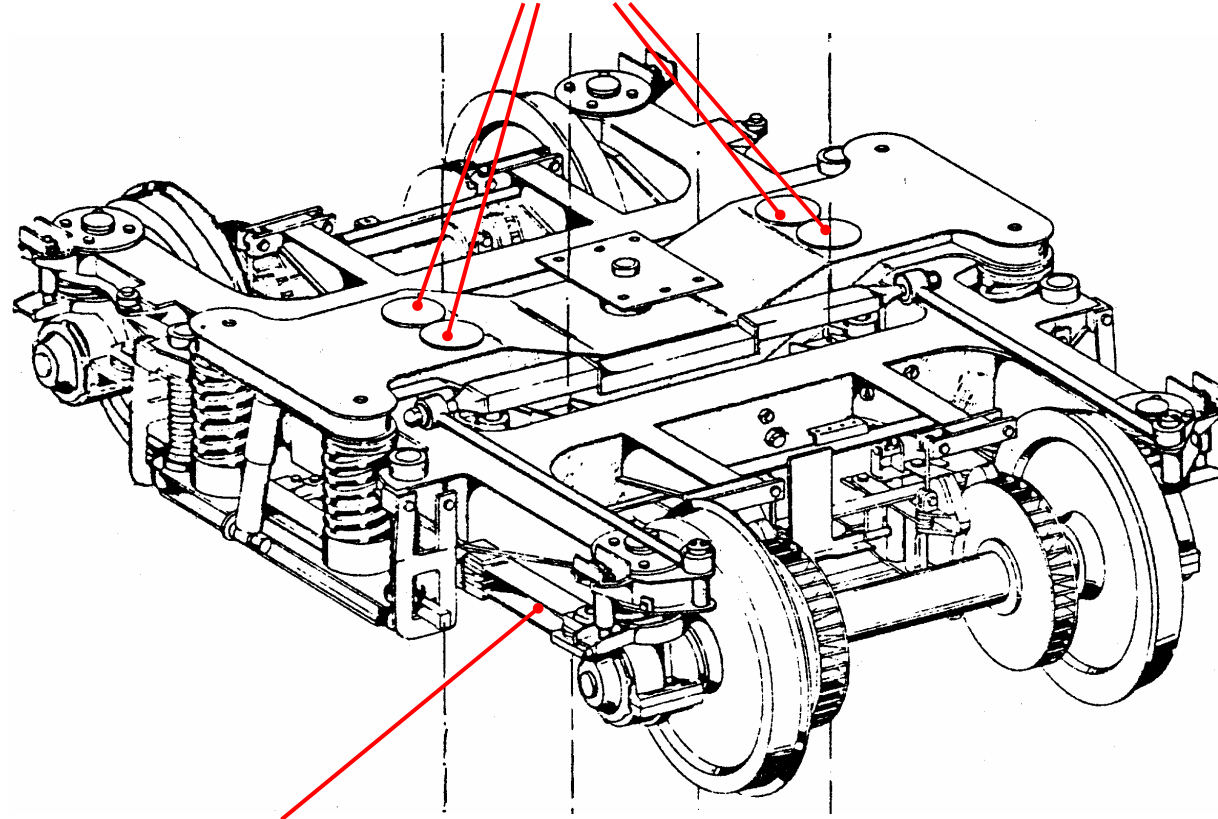
I. Kaiser, K. Popp



# Real system

## Bogie type MD (Minden-Deutz) 522

Yaw damping (friction elements)

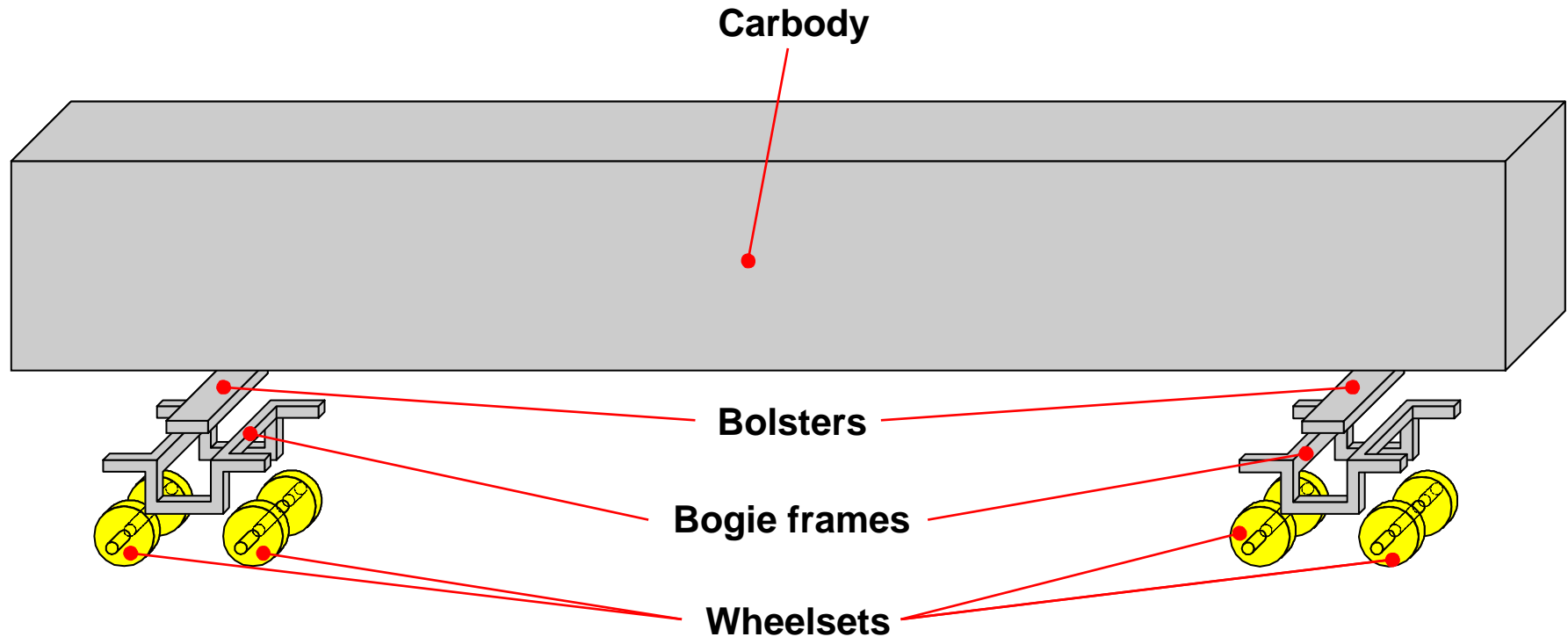


Stiff suspension of the wheelsets

Source: G. Voß, Lecture „Konstruktion der Schienenfahrzeuge“, University of Hannover



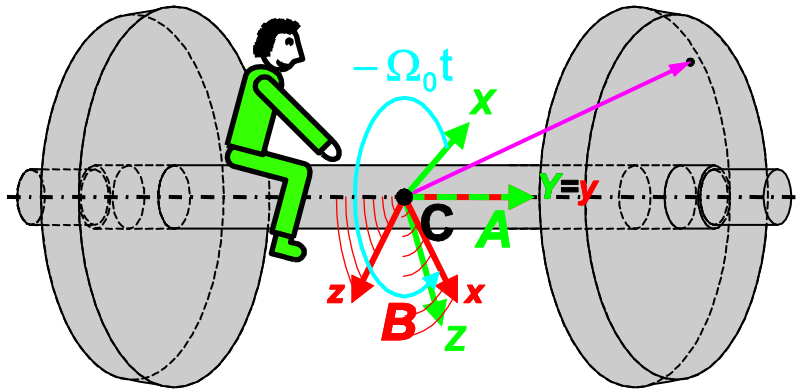
# Structure of the vehicle



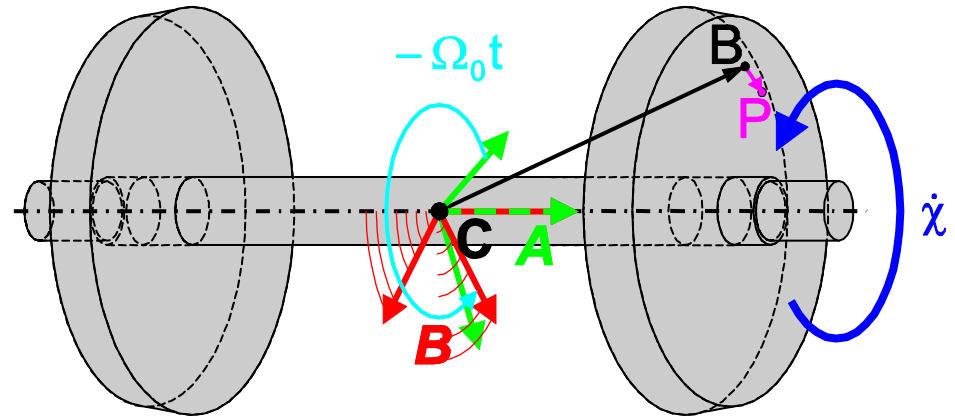
- **Wheelsets:** Elastic bodies with 6 rigid body motions (DoF) + DoFs for deformation
- **Carbody, bogie frames:** Rigid bodies, 6 DoF
- **Bolsters:** Rigid bodies, 1 DoF (yaw motion relative to carbody)
- **Coupling of the bodies by linear spring/damper-elements, exception: yaw damping by dry friction between carbody and bolsters**

# Integration of the rotating elastic wheelsets

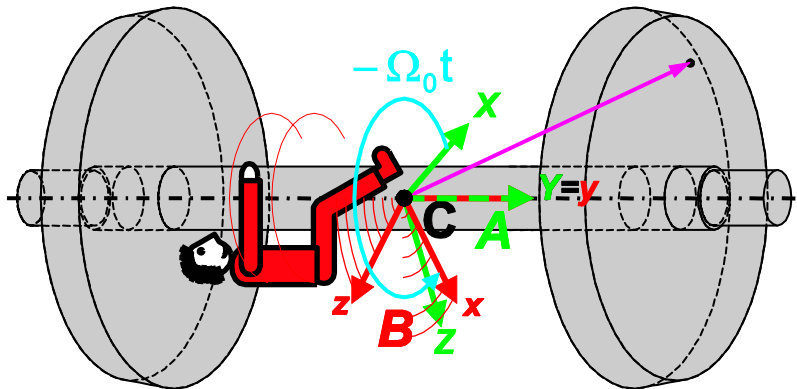
## Eulerian approach



## Arbitrary Lagrangian-Eulerian approach (ALE)



## Lagrangian approach



Modal synthesis in the non-overturning system **A** :

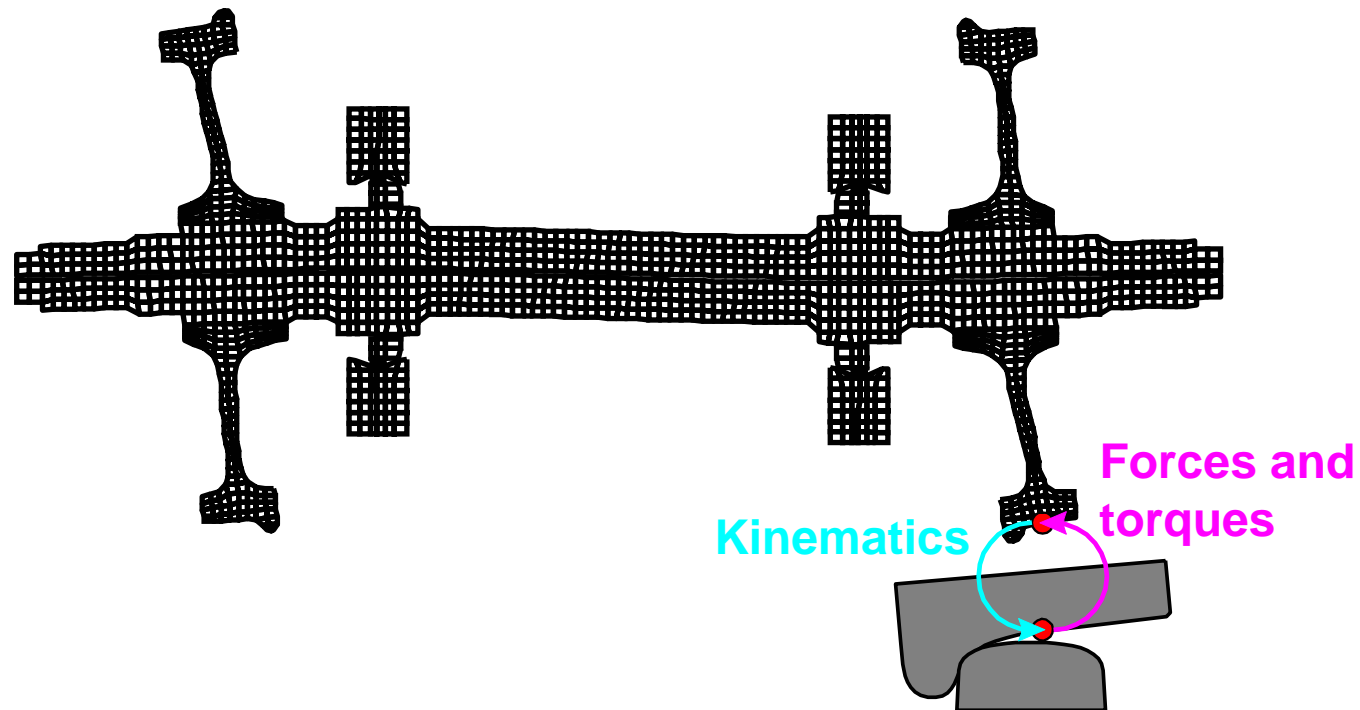
$$\mathbf{r}_{CP}^A = [r \sin \theta \quad y \quad r \cos \theta]^T + \sum_{i=1}^n \mathbf{W}_i(r, \theta, y) q_i(t)$$

Time derivative:

$$\frac{d\mathbf{r}_{CP}^A}{dt} = \frac{\partial \mathbf{r}_{CP}^A}{\partial t} + \frac{\partial \mathbf{r}_{CP}^A}{\partial \theta} \dot{\chi}$$



# Coupling of the elastic wheelset and the contact

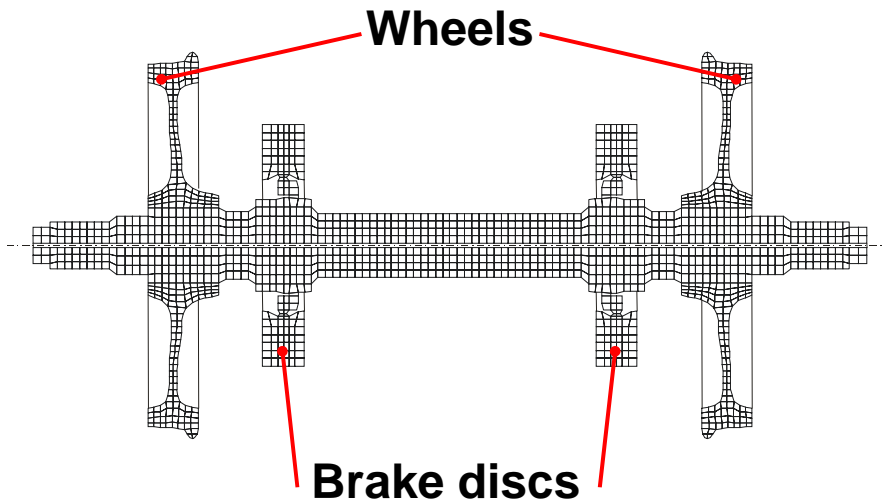


- Application of the **kinematics** from the wheelset on the contact at the **wheel node**
- Application of the **forces** from the contact on the wheelset at the **wheel node**
- Consideration of the shifting of the actual contact by additional **torques**

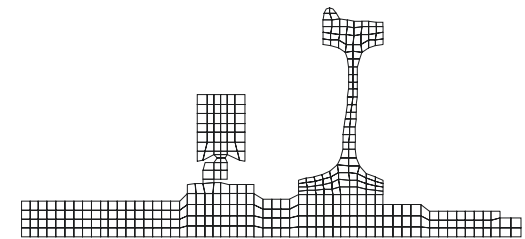


# Finite-Element model of the wheelset

Complete structure



Reduction  
by using  
symmetries



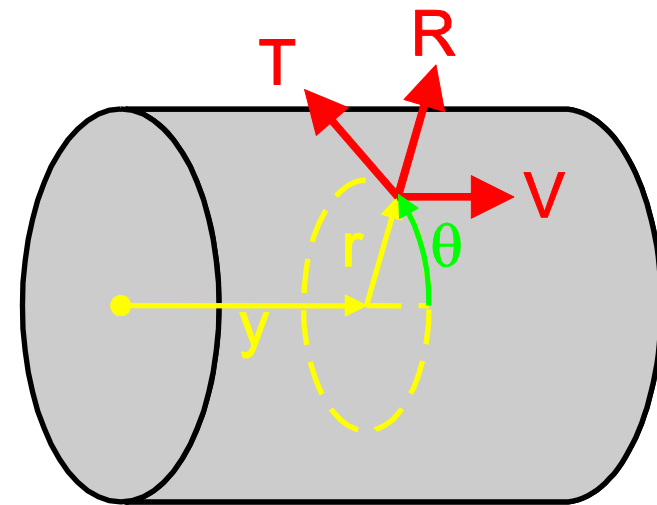
490 nodes,  
1465 or 1460 DoFs

**Semianalytic solution of Navier's equations  
for a rotational symmetric structure**

$$R(r, \theta, y, t) = R_k(r, y) \cos(k\theta + \beta) \cos(\omega_{0,k} t + \varphi)$$

$$T(r, \theta, y, t) = T_k(r, y) \sin(k\theta + \beta) \cos(\omega_{0,k} t + \varphi)$$

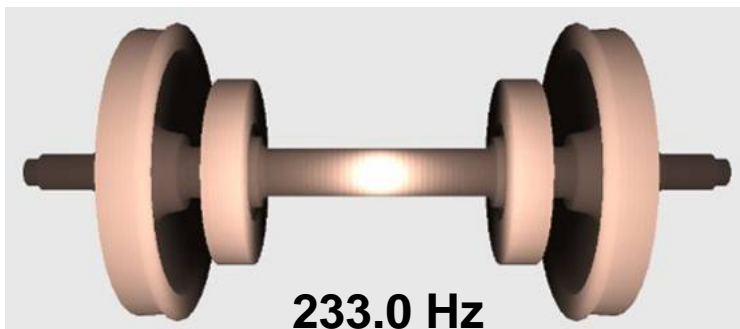
$$V(r, \theta, y, t) = V_k(r, y) \cos(k\theta + \beta) \cos(\omega_{0,k} t + \varphi)$$



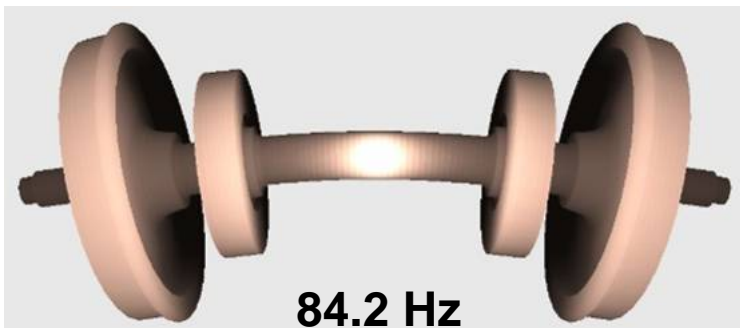
# Results of the FE calculation

## Symmetric modes

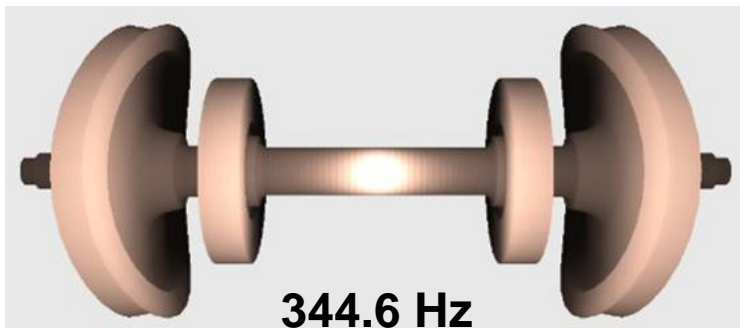
**k=0**  
(umbrella  
modes)



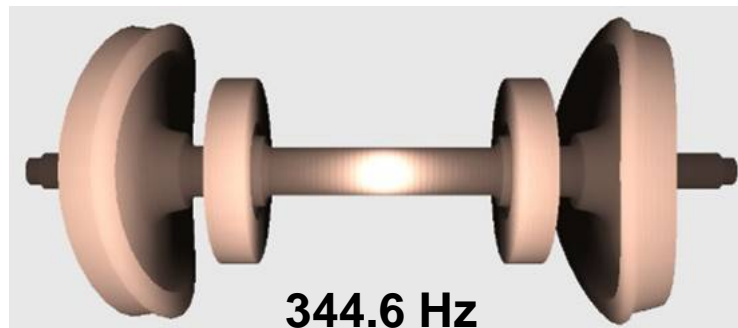
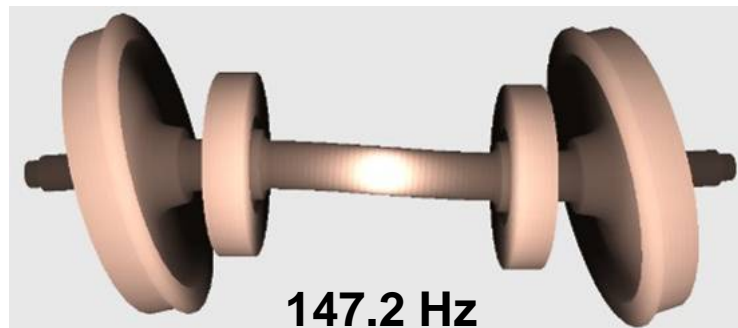
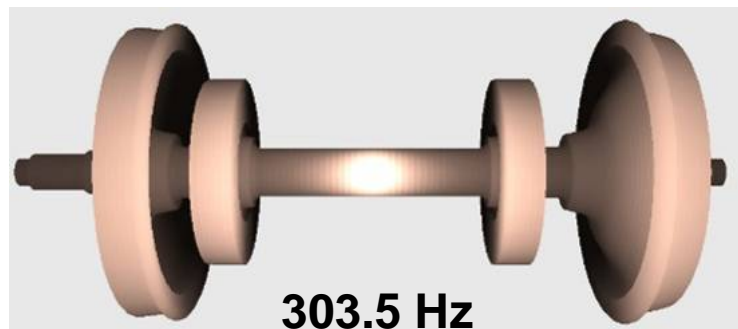
**k=1**  
(bending  
modes)



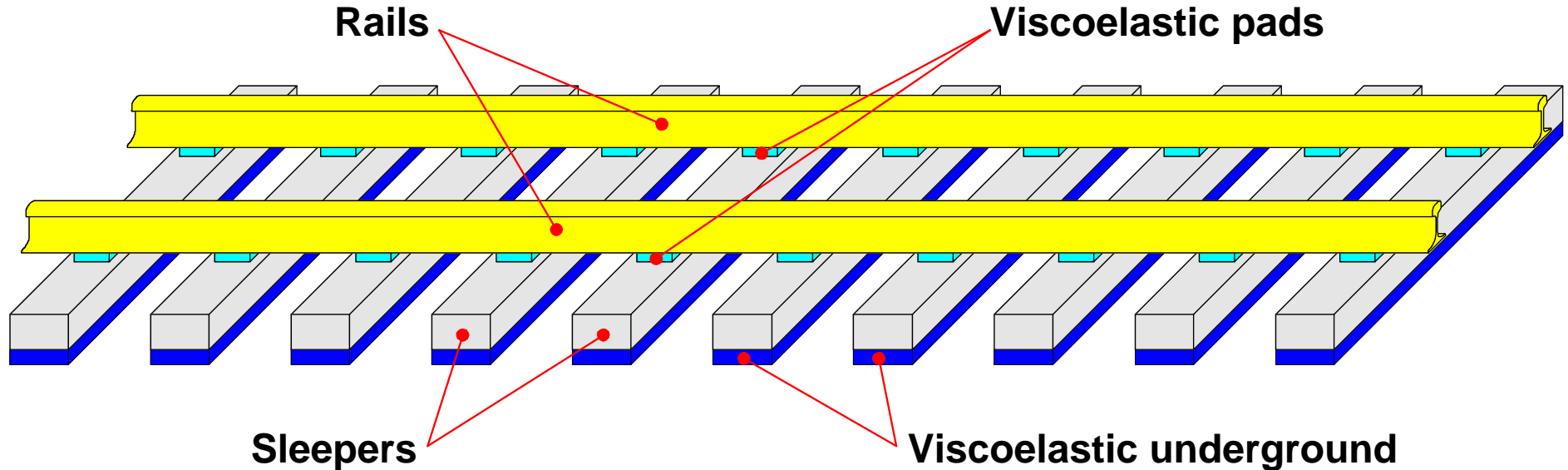
**k=2**  
(wheel  
modes)



## Antisymmetric modes



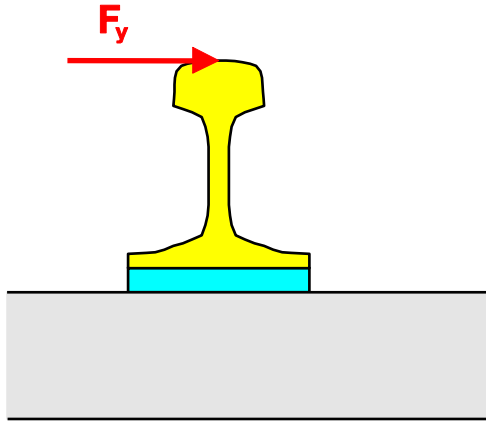
# Structure of the track



- **Rails:** Elastic bodies, identical boundary conditions at the ends
- **Sleepers:** Rigid bodies, 6 DoF, 64 sleepers in total
- **Coupling of the bodies by linear spring/damper elements**
- **Linear system** → *Modal decomposition possible*

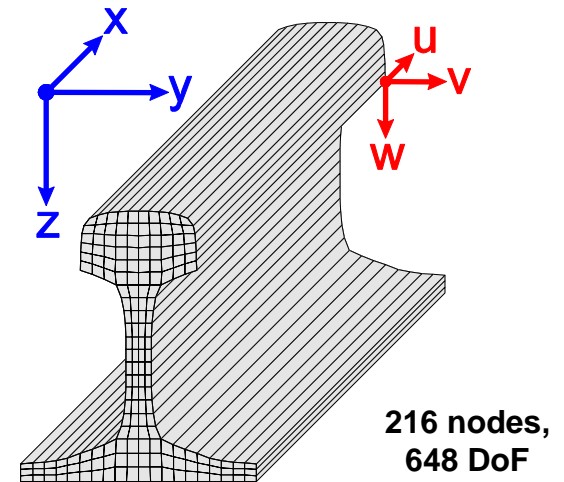
# Modelling of the rail

Eccentric loading of the rail by lateral forces



→ Deformation of the rail's cross section possible

Finite-Element model of the rail



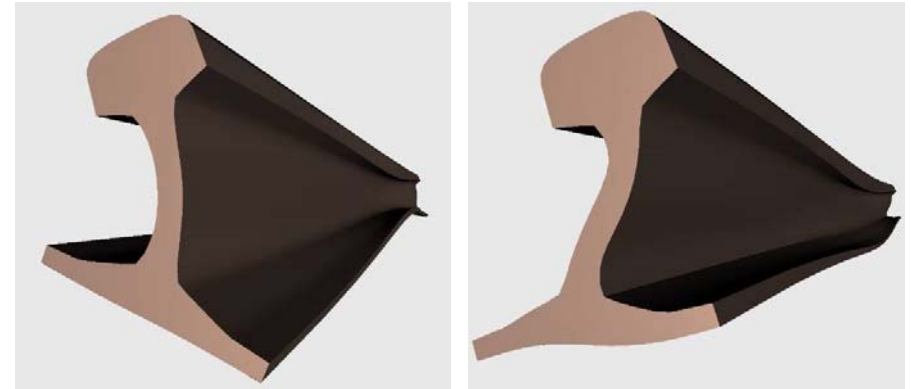
Eigenmodes of the rail

Semianalytic solution of Navier's equations for a prismatic structure

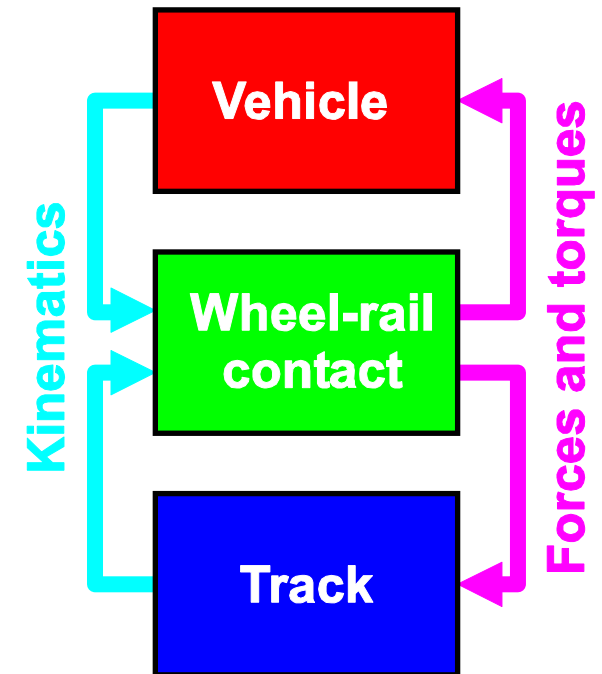
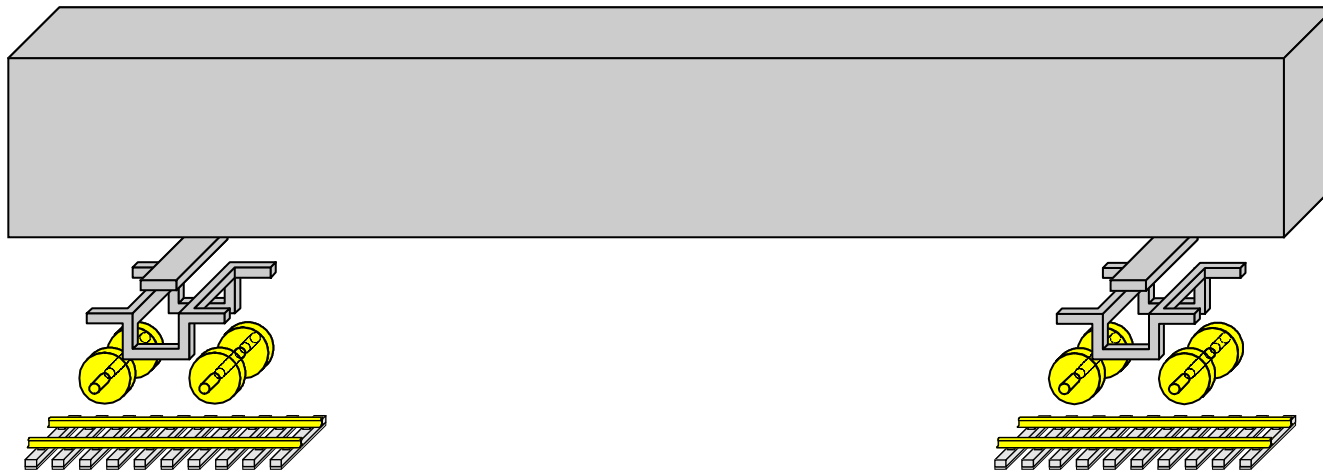
$$u(x, y, z, t) = U_k(y, z) \sin(\kappa_k x + \beta) \cos(\omega_{0,k} t + \varphi)$$

$$v(x, y, z, t) = V_k(y, z) \cos(\kappa_k x + \beta) \cos(\omega_{0,k} t + \varphi)$$

$$w(x, y, z, t) = W_k(y, z) \cos(\kappa_k x + \beta) \cos(\omega_{0,k} t + \varphi)$$



# Vehicle-track system



**Vehicle: Elastic multi-body system (EMBS)**

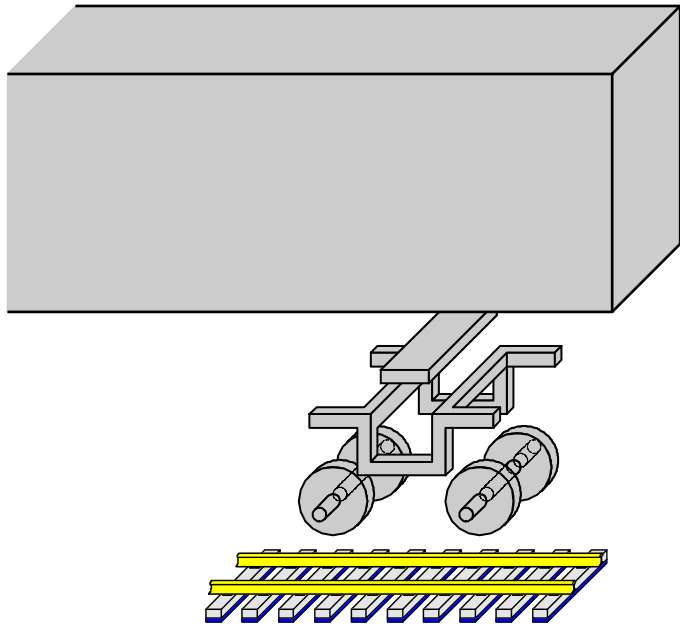
**Wheel-rail contact: Nonlinear force element**

- Nonlinear contact geometry (wheel: S1002, rail: UIC 60, 1/40)
- Nonlinear contact forces  
(normal force: Hertz, tangential forces: Kalker/Polach)

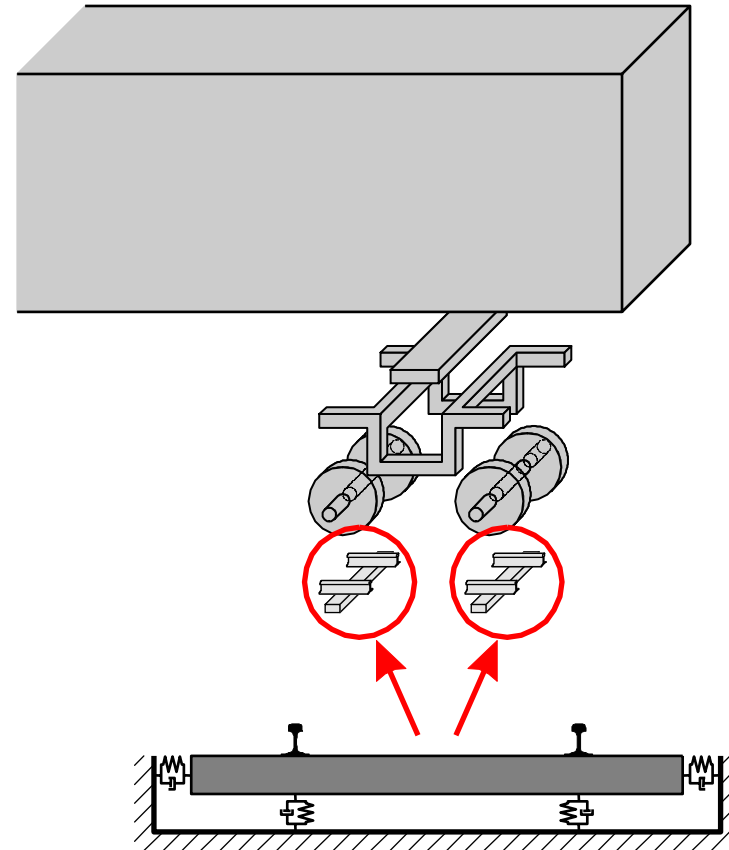
**Track: Discrete-continuous system, two separate tracks, one for each bogie**



# Comparison of track models



Detailed track model („elastic rails“)



Simple track model („rigid rails“)

- 1 rigid track element for each wheelset
- Viscoelastic support of the track element

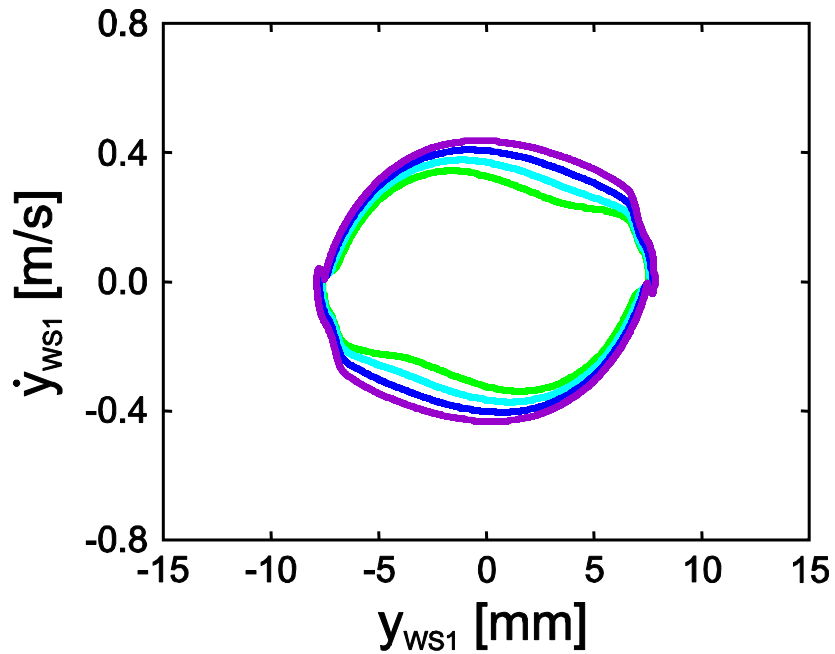




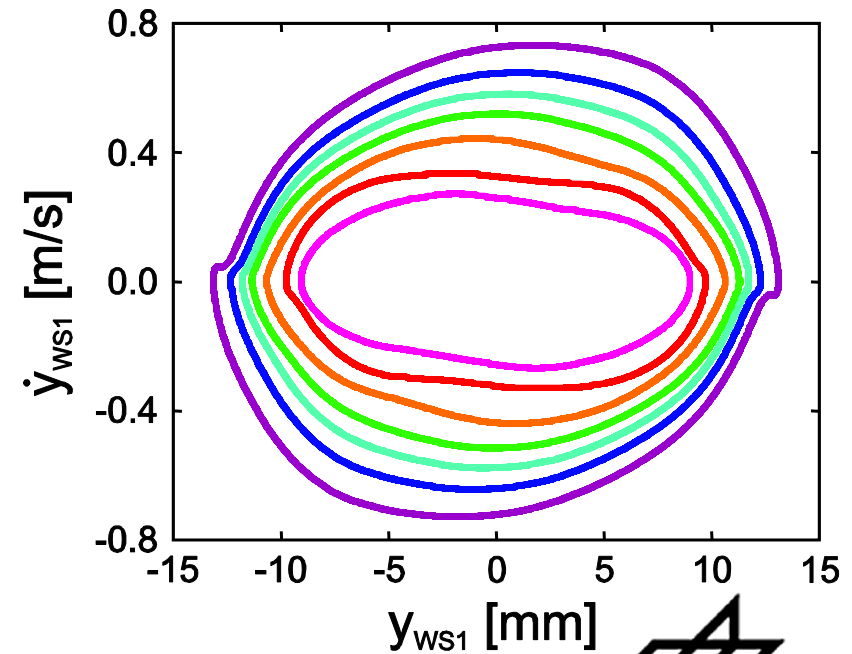
# Influence of the structural elasticity



Rigid wheelsets / rigid rails



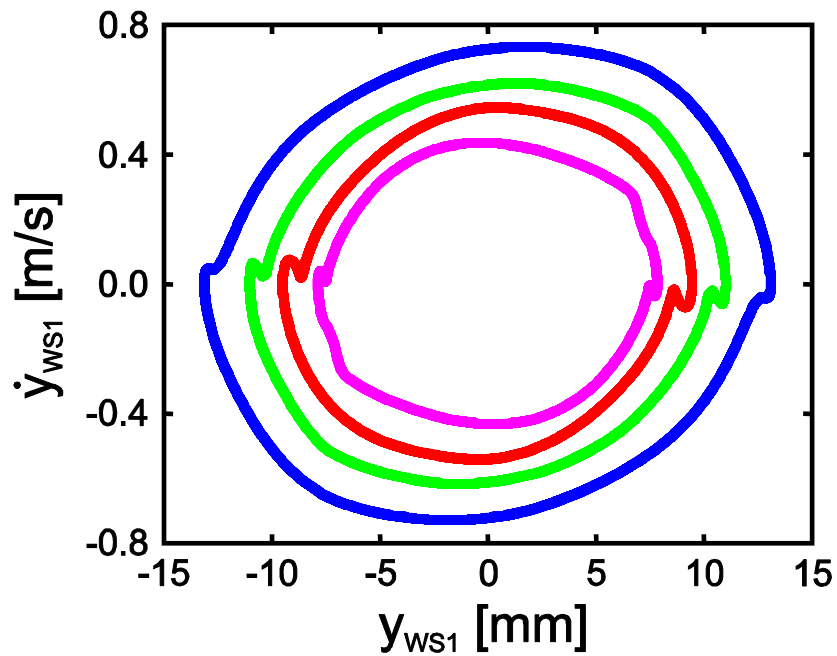
Elastic wheelsets / elastic rails



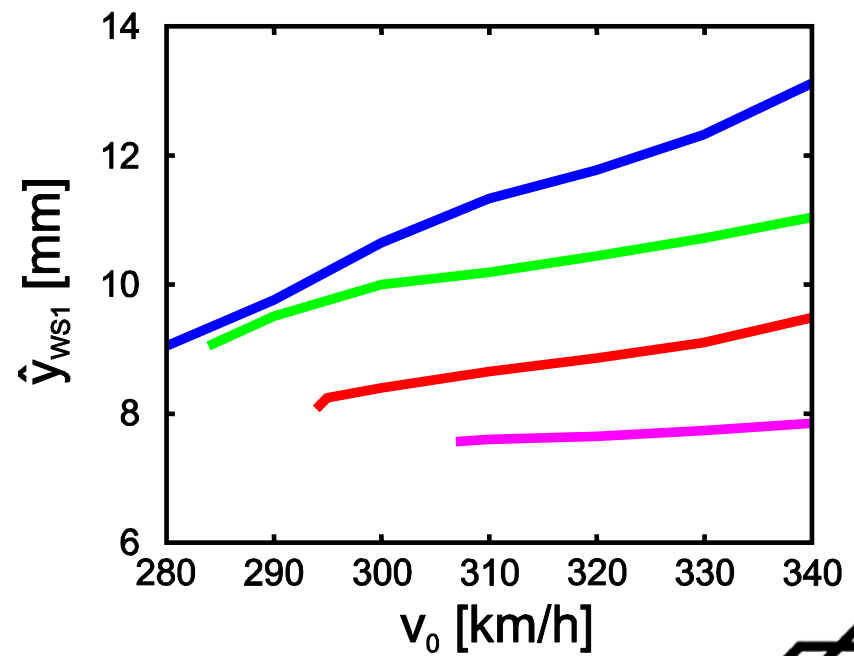
# Influence of different structural elasticities



- Rigid wheelsets / rigid rails
- Rigid wheelsets / elastic rails
- Elastic wheelsets / rigid rails
- Elastic wheelsets / elastic rails



$v_0 = 340$  km/h



---

# Concluding remarks

---

- **Modelling of a passenger coach with elastic wheelsets**
- **Integration of the rotating elastic wheelsets**
- **Semianalytic FE model of the wheelsets (rotational symmetric body)**
- **Modelling of a track with discrete support by sleepers**
- **Semianalytic FE model of the rails (prismatic body)**
- **Structural elasticities lead to lower critical speed of the vehicle and to larger motion amplitudes of the wheelsets**

